

# Cooperative dynamics in the Fiber Bundle Model

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We discuss the cooperative failure dynamics in the Fiber Bundle Model where the individual elements or fibers are Hookean springs, having identical spring constant but different breaking strengths. When the bundle is stressed or strained, especially in the equal-load-sharing scheme, the load supported by the failed fiber gets shared equally by the rest of the surviving fibers. This mean-field type statistical feature (absence of fluctuations) in the load-sharing mechanism helped major analytical developments in the study of breaking dynamics in the model and precise comparisons with simulation results. We intend to present a brief review on these developments.

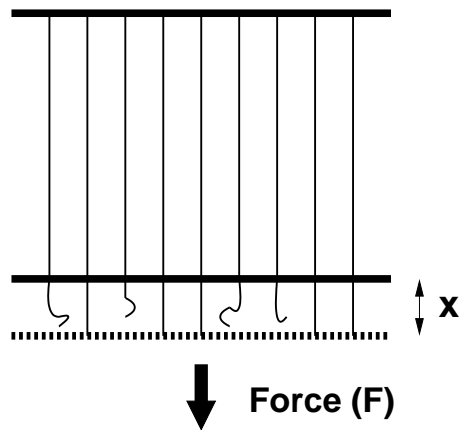


FIG. 1. A cartoon of the Fiber Bundle Model where a macroscopically large number ( $N$ ) of Hookean springs, with identical spring constant but different breaking thresholds hang parallelly from an upper rigid bar and a load/force  $F$  is applied at the lower horizontal rigid bar (not allowing any local deformation of the bar and consequent local stress concentration). If any spring fails at any time, the (extra) load is shared by the surviving fibers at that time. In the equal-load-sharing scheme, considered here, this extra load is shared equally by all the surviving fibers ( $x$  denoting the strain of the surviving fibers).

## I. INTRODUCTION

Fiber bundle model (FBM) has been used widely for studying fracture and failure [1] of composite materials under external loading. The simplicity of the model allow us to achieve analytic solutions [2–4] to an extent that is not possible in any other fracture models. For these very reasons, FBM is widely used as a model of breakdown that extends beyond disordered solids. In fact, FBM was first introduced in connection with textile engineering [5]. Physicists took interest in it recently to explore the critical failure dynamics and avalanche phenomena during such stress-induced failures [6–9]. Apart from the classical fracture-failure in composites, FBM has been used successfully for studying noise-induced (creep/fatigue) failure [10–14] where a fixed load is applied on the system and external noise triggers the failure of elements. Furthermore, it was used as a model for other geophysical phenomena, such as snow avalanche [16], land slides [17, 18], biological materials [19] or even earthquakes [20]. In this review article we want to concentrate only on the cooperative dynamical aspects in FBM.

F. T. Peirce, a textile engineer, introduced the Fiber Bundle Model [5] in 1926 to study the strength of cotton yarns. Later, in 1945 Daniels discussed some static behavior of such a bundle [21] and the model was brought to the attention of physicists in 1989 by Sornette [22] who started analysing the failure process. Even though FBM was designed initially as a model for fracture or failure of a set of parallel elements (fibers), having different breaking thresholds, with the collective load-sharing scheme, the failure dynamics in the model shows all the attributes of the critical phenomena and associated phase transition. It seems, due to the usefulness and richness, FBM plays the same role (in the field of fracture) as the Ising model in magnetism [23].

In FBM, a number of parallel Hookean springs or fibers are clamped between two horizontal platforms (Figure 1). The breaking strengths of the springs or fibers are different. When the load per fiber (stress) exceeds a fiber’s own threshold, it fails. The load it carried has to be shared by the surviving fibers. If the lower platform deforms under loading while upper platform is rigid, fibers in the neighborhood of just-failed fiber will absorb more of the load compared to fibers sitting further away and this arrangement is called local-load-sharing (LLS) scheme [24, 25]. If both the platforms are rigid, the load has to equally distributed among all the surviving fibers, which is called the equal-load-sharing (ELS) scheme. Intermediate load redistribution schemes are also studied (see e.g., [27]) where a part of the load is shared locally within a few fibers and the rest is shared globally among all the fibers.

How does cooperative dynamics set in? In case of ELS, all the intact fibers carry the load equally. When a fiber fails, the stress level increases on the remaining fibers and that can trigger more fiber-failures (successive failure). As long as the initial load is low, the successive failures of the fibers remain small and though the strain (stretch) of the bundle grow with increasing stress (load), the bundle as a whole does not fail. Once the initial load reaches a “critical” value, determined by the fiber strength distribution, the successive failures become a global (catastrophic) one and the bundle collapses.

We arrange this review article as follows: In the short introduction (section I), we elaborate the concept of the

fiber bundle model and its evolution as a fracture model. Section II deals with the equal-load-sharing FBM where we demonstrate the dynamical behavior in FBM with evolution dynamics and their solutions. Analytic results are compared with numerical simulations in this section. In section III we discuss noise-induced failure dynamics in FBM through theory, simulation and real-data analysis. The self-organizing mechanism in FBM is discussed in section IV. We reserve section V for discussions on some works which would help to understand the cooperative dynamics in FBM. Finally, we keep a short Summary and Conclusion section (section VI) at the end.

## II. EQUAL LOAD SHARING FBM

We consider a FBM having  $N$  parallel fibers placed between two rigid bars. Each fiber follows Hook's law with a force  $f$  to the stretch value  $x$  as  $f = \kappa x$ , where  $\kappa$  is the spring constant. To make things simpler, we consider  $\kappa = 1$  for all the fibers. Each fiber has a particular strength threshold value and if the stretch  $x$  exceeds this threshold, the fiber fails irreversibly. We are interested in the equal-load-sharing (ELS) mode (the bars are rigid), and by construction of the model, the applied load has to be shared equally by the intact fibers.

Other than the analytical treatment of the model, several aspects of the model are also explored numerically. The implementation of the model, particularly in the equal load sharing version we discuss here, is straightforward. The load is initially applied to each fiber equally. The fibers having failure thresholds less than the applied load are irreversibly broken. The load carried by those fibers is redistributed equally among the remaining fibers, which can cause further breaking. The redistribution continues until no new fibers are breaking. The external load is held constant during the whole redistribution process. This is due to the separation of time scales of externally applied loading rate and the internal (elastic) relaxation processes within materials. After the end of each redistribution cycle, the external load is further increased to continue the dynamics. This process continues until the entire system is broken. The critical strength, avalanche statistics and other critical exponents are calculated from this dynamics, which as will see, match well with the analytical results.

### A. Fiber strength distributions

The fiber strength thresholds are drawn from a probability density  $p(x)$ . The corresponding cumulative probability is

$$P(x) = \int_0^x p(y)dy . \quad (1)$$

The most used threshold distributions are uniform and Weibull distributions (see Figure 2) in FBM literature.

For a uniform distribution we can write

$$p(x) = 1; P(x) = x, \quad (2)$$

where the range of function is between 0 to 1. The cumulative Weibull distribution has a form:

$$P(x) = 1 - \exp(-x^k), \quad (3)$$

where,  $k$  is the shape parameter or Weibull index. The corresponding probability distribution takes the form:

$$p(x) = kx^{k-1} \exp(-x^k). \quad (4)$$

The shape of the uniform and Weibull distributions are shown in Figure (2). The range of definition is between 0 to  $\infty$ .

### B. The critical values

When we stretch the bundle by applying a force, the fibers fail according to their thresholds, the weakest first, then the next weakest and so on. If  $N_f$  fibers have failed at a stretch value  $x$ , the force on the bundle is

$$F = (N - N_f)x = N(1 - P(x))x, \quad (5)$$

as  $\kappa = 1$ . The normalized force ( $F/N$ ) vs. stretch  $x$  curve looks like a parabola (Figure 3).

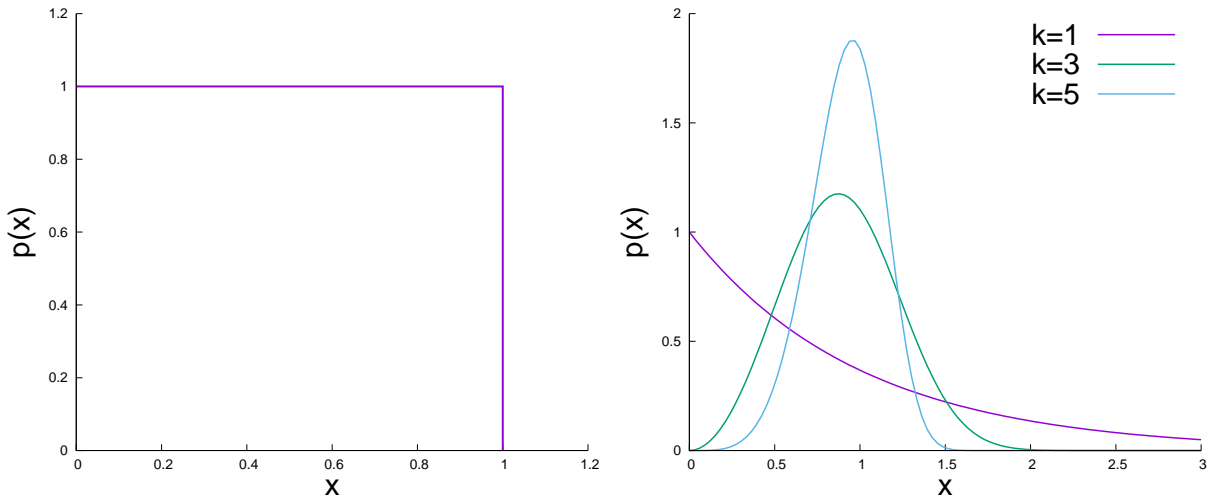


FIG. 2. The uniform and Weibull distributions of fiber strengths (thresholds).

It is obvious that the maximum of the force value is the strength of the bundle and the corresponding stretch value ( $x_c$ ) is called the critical stretch beyond which the bundle collapses. Therefore, we can define two distinct phases of the system: stable phase for  $0 < x \leq x_c$  and unstable phase for  $x > x_c$ .

The critical stretch value can be obtained easily by setting  $dF(x)/dx = 0$ :

$$1 - x_c p(x_c) - P(x_c) = 0. \quad (6)$$

### 1. Uniform threshold distribution

Substituting the  $p(x_c)$  and  $P(x_c)$  values for uniform distribution, we obtain

$$x_c = \left(\frac{1}{2}\right). \quad (7)$$

Now inserting the  $x_c$  value in the force expression (Eq. 5), we get

$$\frac{F_c}{N} = \frac{1}{4}; \quad (8)$$

which is the critical strength of the bundle (Figure 3).

### 2. Weibull threshold distribution

In case of Weibull distribution, at the force-maximum, inserting the  $P(x)$ ,  $p(x)$  values into expression (Eq. 6), we obtain

$$\exp(-x_c^k) - (x_c k x_c^{k-1} \exp(-x_c^k)) = 0. \quad (9)$$

One can get the critical stretch value:

$$x_c = k^{-\frac{1}{k}}; \quad (10)$$

and the corresponding critical force value

$$\frac{F_c}{N} = k^{-\frac{1}{k}} \exp\left(-\frac{1}{k}\right). \quad (11)$$

For  $k = 1$ ,  $x_c = 1.0$  and  $\frac{F_c}{N} = \frac{1}{e}$  (Figure 3).

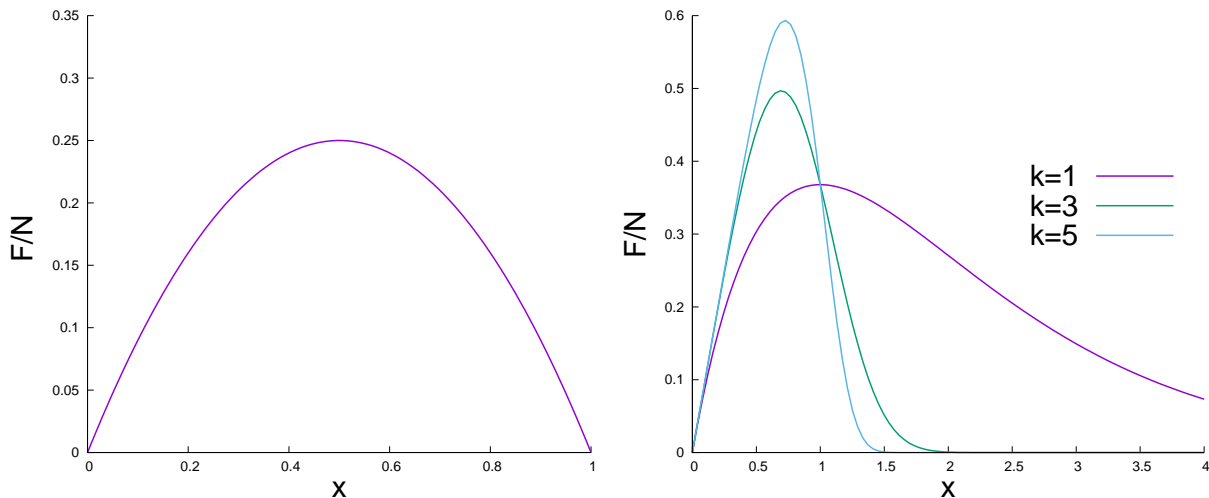


FIG. 3. Normalized force ( $F/N$ ) against extension  $x$  for a fiber bundle with uniform ( $x_c = 0.5$ ) and Weibull ( $x_c = 1, (1/3)^{1/3}, (1/5)^{1/5}$  for  $k = 1, 3, 5$  respectively) distributions of strengths (thresholds).

### C. Different ways of loading

Now we will discuss how the load or stress on the bundle can be applied. In the FBM literature, the most common loading mechanism discussed [28, 29] is the “weakest-link-failure” mechanism of loading. This loading process ensures a separation in time scales between external loading and internal stress redistribution. This is equivalent to a “quasi-static” approach and noise/fluctuation in the threshold distribution influences the breaking dynamics as well as the avalanche statistics.

A fiber bundle can also be loaded in a different way by applying a fixed amount of load at a time. In that case, all fibers having failure threshold below the applied load, fail. The stress on the surviving fibers then increases due to load redistribution. The increased stress may drive further failures, and so on. This iterative breaking process continues until an equilibrium is reached where the intact fibers (those who can support the load) is reached. One can also study the failure dynamics of the bundle when the external load on the bundle is then increased infinitesimally, but by a fixed amount (irrespective of the fluctuations in the fiber strength distribution as discussed above). Indeed, as shown recently in Biswas and Chakrabarti [52], the universality class of the dynamics of such fixed loading (even for the same ELS mode of load redistribution after individual fiber failure) will be different from that for the quasi-static (or weakest link failure type) loading discussed above and is given by the Flory statistics [54] for linear polymers, accommodating the Kolmogorov type dispersion in turbulence [55].

### D. The cooperative dynamics

We are going to discuss now the cooperative dynamical behavior of the breaking processes for the bundle loaded by fixed amount per step (following the formulations in the References [1, 2, 4, 8, 28, 29, 31]).

Let us assume that an external force  $F$  is applied to the fiber bundle. The stress on the bundle (the external load per fiber) is

$$\sigma = F/N. \quad (12)$$

Let us call  $N_t$  be the number of surviving fibers after  $t$  steps in the stress redistribution cycle, with  $N_0 = N$ .

The effective stress becomes

$$\sigma_t = N\sigma/N_t. \quad (13)$$

Therefore,  $NP(N\sigma/N_t)$  of fibers will fail in the first stress redistribution cycle. The number of intact fibers in the next cycle will be

$$N_{t+1} = N - NP(N\sigma/N_t). \quad (14)$$

Using  $n_t = N_t/N$ , Eq. (14) takes the form of a recursion relation,

$$n_{t+1} = 1 - P(\sigma/n_t), \quad (15)$$

with  $\sigma$  as the control parameter and  $n_0 = 1$  is the start value.

The character of an iterative dynamics is determined by its *fixed points* (denoted by  $*$ ) where a dynamical variable remains exactly at the same value it had in the previous step of the dynamics. In other words, a fixed point is a value (of a dynamical variable) that is mapped onto itself by the iteration. The dynamics stops or it becomes locked at the fixed point.

One can find out the possible fixed points  $n^*$  of (15), which satisfy

$$n^* = 1 - P(\sigma/n^*), \quad (16)$$

and the solutions of the breaking dynamics at the fixed point.

### E. The critical exponents

If we consider that the fiber strengths follow uniform distribution, the recursion relation can be written as

$$n_{t+1} = 1 - \sigma/n_t. \quad (17)$$

Consequently, at the fixed point the relation assumes a simple form

$$(n^*)^2 - n^* + \sigma = 0, \quad (18)$$

with solution

$$n^* = \frac{1}{2} \pm (\sigma_c - \sigma)^{1/2}. \quad (19)$$

Here critical stress value  $\sigma_c = 1/4$ , beyond which the bundle collapses completely. In (19) the upper sign gives  $n^* > n_c$  which corresponds to a stable fixed point. From this solution, it is easy to derive the order parameter, susceptibility and relaxation time (all defined below).

The fixed-point solution gives the critical value: ( $\sigma = \sigma_c$ )

$$n_c^* = \frac{1}{2}. \quad (20)$$

Therefore, the fixed-point solution can be presented as

$$n^*(\sigma) - n_c^* \propto (\sigma_c - \sigma)^\beta, \quad \beta = \frac{1}{2}. \quad (21)$$

Clearly,  $n^*(\sigma) - n_c^*$  can be considered like an *order parameter*, which shows a clear transition from non-zero to zero value at  $\sigma_c$ .

The *susceptibility* is defined as  $\chi = -dn^*/d\sigma$  and the fixed-point solution gives

$$\chi \propto (\sigma_c - \sigma)^{-\gamma}, \quad \gamma = \frac{1}{2}; \quad (22)$$

which follows a power law and diverges at the critical point  $\sigma_c$ .

The dynamical approach very near a fixed point is very interesting and this can be investigated by expanding the differences  $n_t - n^*$  around the fixed point. In case of uniform distribution, the recursion relation (17), gives

$$n_{t+1} - n^* = \frac{\sigma}{n^*} - \frac{\sigma}{n_t} = \frac{\sigma}{n_t n^*} (n_t - n^*) \simeq \frac{\sigma}{n^{*2}} (n_t - n^*). \quad (23)$$

Clearly, the fixed point is approached with exponentially decreasing steps:

$$n_t - n^* \propto e^{-t/\tau}, \quad (24)$$

where  $\tau$  is a relaxation parameter, dependent on stress value:

$$\tau = 1/\ln(n^{*2}/\sigma) = 1/\ln \left[ \left( \frac{1}{2} + \sqrt{\frac{1}{4} - \sigma} \right)^2 / \sigma \right]. \quad (25)$$

At the critical stress,  $\sigma = \sigma_c = \frac{1}{4}$ , the argument of the logarithm is 1 and apparently  $\tau$  is infinite. As the critical stress is approached, for  $\sigma \rightarrow \sigma_c$

$$\tau \simeq \frac{1}{4} (\sigma_c - \sigma)^{-\theta} \quad \text{with} \quad \theta = \frac{1}{2}. \quad (26)$$

This divergence clearly shows the character of the breaking dynamics, i.e., it becomes very very slow at at the critical point.

### F. Universal behavior

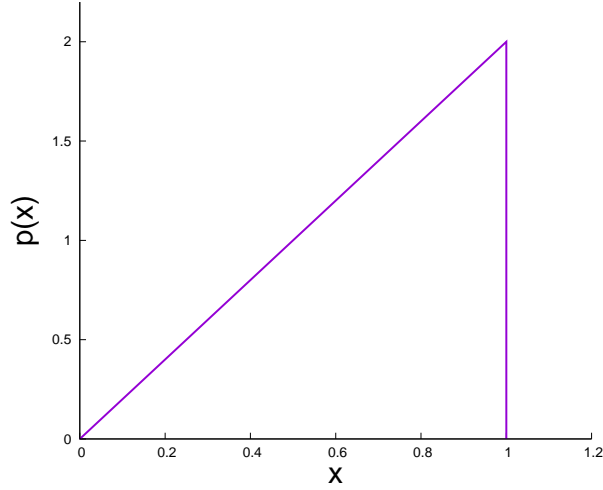


FIG. 4. The linearly increasing fiber strength distribution.

The recursion relation and the fixed point solutions demonstrated the dynamic critical behavior for the uniform distribution of the breaking thresholds. Now the question arises -how general the results are? The *universality* of the cooperative breaking dynamics can be verified by considering a different distribution of fiber strengths. We are now going to examine the situation for a *linearly increasing distribution* (Figure 4) within the interval  $(0, 1)$ ,

$$p(x) = \begin{cases} 2x, & 0 \leq x \leq 1 \\ 0 & x > 1. \end{cases} \quad (27)$$

From the force-stretch relationship, the average force per fiber is

$$F(x)/N = \begin{cases} x(1-x^2) & 0 \leq x \leq 1 \\ 0 & x > 1, \end{cases} . \quad (28)$$

Therefore, the critical point is

$$\sigma_c = \frac{2}{3\sqrt{3}}. \quad (29)$$

In this case the breaking dynamics can be written as a recursion relation:

$$n_{t+1} = 1 - (\sigma/n_t)^2, \quad (30)$$

and the fixed-point equation is

$$(n^*)^3 - (n^*)^2 + \sigma^2 = 0, \quad (31)$$

i.e., a cubic equation in  $n^*$ . Clearly, there are three solutions of  $n^*$  for a value of  $\sigma$ . At the critical stress value,  $\sigma_c = 2/3\sqrt{3}$ , the only acceptable solution of (31) is

$$n_c^* = \frac{2}{3}. \quad (32)$$

We want to investigate the breaking dynamics in the neighborhood of the critical point. Therefore, we insert  $n = \frac{2}{3} + (n - n_c)$  into (30), with the result

$$\frac{4}{27} - (n - n_c)^2 - (n - n_c)^3 = \sigma^2 = \left(\frac{2}{3\sqrt{3}} + \sigma - \sigma_c\right)^2 = \frac{4}{27} + \frac{4}{3\sqrt{3}}(\sigma - \sigma_c) + (\sigma - \sigma_c)^2. \quad (33)$$

We get (to leading order)

$$(n - n_c)^2 = \frac{4}{3\sqrt{3}}(\sigma_c - \sigma). \quad (34)$$

Obviously, for  $\sigma \leq \sigma_c$  the *order parameter* behaves as

$$n(\sigma) - n_c \propto (\sigma_c - \sigma)^\beta, \quad \beta = \frac{1}{2}, \quad (35)$$

in accordance with (21). The *susceptibility*  $\chi = -dn/d\sigma$  gives

$$\chi \propto (\sigma_c - \sigma)^{-\gamma}, \quad \gamma = \frac{1}{2}. \quad (36)$$

We can also discuss how the stable fixed point is approached from below. From (30) one can write, around the fixed point

$$n_{t+1} - n^* = \frac{\sigma^2}{n^{*2}} - \frac{\sigma^2}{n_t^2} = \frac{\sigma^2}{n^{*2}n_t^2} (n_t^2 - n^{*2}) \simeq (n_t - n^*) \frac{2\sigma^2}{n^{*3}}. \quad (37)$$

The approach is clearly exponential,

$$n_t - n^* \propto e^{-t/\tau} \quad \text{with} \quad \tau = \frac{1}{\ln(n^{*3}/2\sigma^2)}. \quad (38)$$

The argument of the logarithm becomes 1 exactly at the critical point, therefore  $\tau$  diverges when the critical state is approached. The nature of such divergence assumes the same form,

$$\tau \propto (\sigma_c - \sigma)^{-\theta}, \quad \theta = \frac{1}{2}, \quad (39)$$

which is similar to the model with a uniform fiber strengt distribution, Eq. (26).

We can now conclude that, the ELS FBM with a linearly increasing fiber strength distribution possesses the same critical power laws as the ELS FBM with a uniform fiber strength distribution. This confirms that the critical properties of the cooperative breaking dynamics are universal. A general treatment for verifying universality in ELS FBM can be found in Reference [28].

## G. Two-sided critical divergence

When fixed amount of load is applied on the system, the iterative breaking process ends with one of two possible end results. Either the whole bundle collapses, or an equilibrium situation is reached where intact fibers can hold/support the applied load/stress. Thus, the final fate of the bundle depends on whether the external stress  $\sigma$  on the bundle is postcritical ( $\sigma > \sigma_c$ ), precritical ( $\sigma < \sigma_c$ ), or critical ( $\sigma = \sigma_c$ ). It is interesting to know how the breaking dynamics is approaching the critical point (failure point) from below (pre-critical) and above (post-critical) stress values.

In case of uniform fiber strength distribution when the external stress approaches the critical value  $\sigma_c = 1/4$  from a higher value, i.e., in the post-critical region, the number of necessary iterations needed for the whole system to break increases as the critical point is approached. Close to the critical point, number of iterations shows a square-root divergence [8]:

$$t_f \simeq \frac{1}{2}\pi(\sigma - \sigma_c)^{-1/2}. \quad (40)$$

Similarly, in the pre-critical region, when the external stress approaches the critical value  $\sigma_c = 1/4$  from below, the number of iterations has again a square root divergence [8] (for uniform distribution) close to the critical point:

$$t_f = \frac{1}{4} \ln(N) (\sigma_c - \sigma)^{-1/2}. \quad (41)$$

The only difference is that, in pre-critical case, the amplitude of the square root divergence has a system-size-dependence which is absent in post-critical case.

We can conclude that in ELS FBM, the breaking dynamics shows a two-sided critical divergence in terms of the number of iteration steps needed to reach critical point from below (pre-critical) and above (post-critical) (Figure 5). The theoretical details of the exact solutions can be found in References [8, 28].

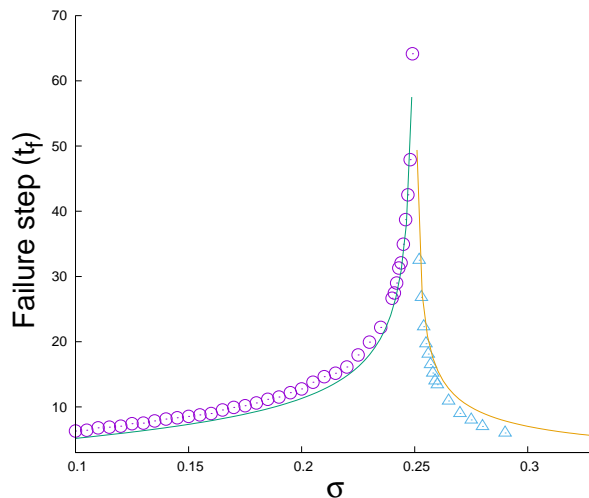


FIG. 5. Post-critical and pre-critical relaxation: Numerical data are for a bundle with  $N = 10^6$  fibers having uniform threshold distribution and averages are taken over  $10^5$  samples. Lines are showing theoretical estimates.

### H. Avalanche dynamics with fixed amount loading

The number of fibers ( $S$ ) breaking between two successive stable conditions of the fiber bundle is called an avalanche. The distribution of the avalanche sizes  $P(S)$  shows a power-law tail for the large  $S$  limit [6], which is a sign of the criticality discussed above. This is experimentally widely observed for driven disordered systems in general [31] and (quasi-brittle/ductile) fracture in particular. While the details of the avalanche dynamics seen in the fiber bundle model with quasi-static load increase has been discussed elsewhere in this special issue [30], here we briefly describe the avalanche dynamics for fixed amount load increase i.e., when the system is in a stable condition, a fixed amount of load  $\delta$  is added, which restarts the dynamics. As before, the number of fibers breaking until the system reaches the next stable state constitutes an avalanche. Clearly, this type of avalanche is a result of the cooperative breaking dynamics and it is not arising due to any fluctuations in stress levels or in fiber strength distribution. We will describe below how to calculate theoretically the distribution of such avalanches:

The load curve, in terms of the threshold values, can be written as

$$F(x) = Nx(1 - x) \quad (42)$$

for uniform threshold distribution in  $(0, 1)$  (see Eq. (5)). The load increases between 0 and  $N/4$  with increment  $\delta$ . Therefore, the values of the load are  $m\delta$ , with  $m = 0, 1, 2, \dots, N/4\delta$ . The threshold value for load  $m\delta$  can be obtained from Eq. (42) as

$$x_m = \frac{1}{2}(1 - \sqrt{1 - 4m\delta/N}). \quad (43)$$

The average number of fibers broken due to the increase of load from  $m\delta$  to  $(m + 1)\delta$  is

$$S = N \frac{dx_m}{dm} = \frac{\delta}{\sqrt{1 - 4m\delta/N}}. \quad (44)$$

The number of avalanches of size between  $S$  and  $S + dS$  is obtained from the corresponding interval of the variable  $m$  i.e.,  $P(S)dS = dm$ . From the equation above, we have

$$\frac{dS}{dm} = 2S^3/(N\delta). \quad (45)$$

Therefore, the avalanche size distribution is given by

$$P(S) = \frac{dm}{dS} = \frac{1}{2}N\delta S^{-3}, \text{ for } S \geq \delta. \quad (46)$$

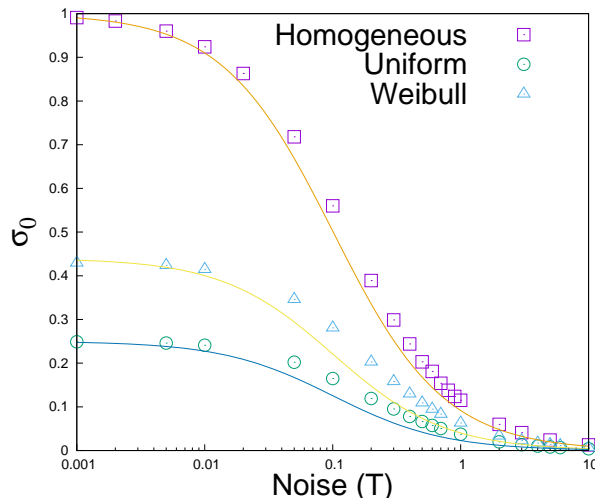


FIG. 6. Phase boundary ( $\sigma_0$  vs.  $T$  plot) for three different type of fiber strength distributions with  $N = 20000$ . Data points are simulation results and solid lines are analytic estimates (Eq. 50) based on mean-field arguments.

Indeed, it is possible to show [28] that for an arbitrary threshold distribution  $p(x)$ , the large  $S$  asymptotic limits of the avalanche size distribution is

$$P(S) \sim CS^{-3}, \quad (47)$$

with  $C = N\delta \frac{p(x_c)^2}{2p(x) + x_c p'(x_c)}$ , with the mild assumption that the load curve has a generic parabolic form with a critical point.

### III. NOISE-INDUCED FAILURE IN FBM

So far we have discussed the classical stress-induced failure of fibers without the presence of noise. A noise-induced failure scheme for fiber bundle model can be formulated [13–15] for which the cooperative failure dynamics can be solved analytically.

As in the previous sections, we consider a bundle of  $N$  parallel fibers clamped between two rigid bars. A load or force ( $F = \sigma N$ ) is applied on the bundle. The fibers have different strength thresholds ( $x$ ) and there is a critical strength  $\sigma_c$  [1] for the whole bundle, so that the bundle does not fail completely for stress  $\sigma \leq \sigma_c$ , but it fails immediately for  $\sigma > \sigma_c$ . Now we introduce noise ( $T$ ) in the system and assume that each fiber having strength  $x_i$  has a finite probability  $P_f(\sigma, T)$  of failure at any stress  $\sigma$  induced by a noise  $T$ :

$$P_f(\sigma, T) = \begin{cases} C \exp\left[-\frac{1}{T} \left(\frac{x_i}{\sigma} - 1\right)\right], & 0 \leq \sigma \leq x_i \\ 1, & \sigma > x_i \end{cases} \quad (48)$$

Here  $C$  is a prefactor.  $P_f(\sigma, T)$  increases as  $T$  increases and for a fixed value of  $T$  and  $\sigma_c$ , as we increase  $\sigma$ , the bundle breaks more rapidly. The motivation behind Eq. (48) comes from the time-dependent behavior or so-called creep behavior of materials, observed in real systems [10, 28]. It is obvious that strength of elements/fibers degrades in time due to external influences like moisture, temperature etc.

Such a noise-induced failure scheme will produce two different failure regimes depending on the stress and noise levels -continuous breaking regime and intermittent breaking regime. In the continuous breaking regime we can calculate the failure time (step) as a function of stress and noise values. However, in the intermittent breaking regime one can define the waiting time between two consecutive failure phases.

The phase boundary can be determined through a mean-field argument that at  $\sigma = \sigma_0$ , at least one fiber must break to trigger the continuous fracturing process. After this single failure the applied load has to be redistributed on the intact fibers (due to ELS) and the effective stress will surely increase (more than  $\sigma_0$ ), which in turn enhances failure probability for all the intact fibers. Following this logic, in case of homogeneous bundle where all the fibers have identical strength  $x_i = 1$  (and  $\sigma_c = 1$ ), at the phase boundary  $NP_f(\sigma_0, T) \geq 1$  giving

$$N \exp\left[-\frac{1}{T} \left(\frac{1}{\sigma_0} - 1\right)\right] \geq 1 \quad (49)$$

which finally gives

$$\sigma_0 \geq \frac{1}{1 - T \log(1/N)}. \quad (50)$$

In absence of noise, when  $T = 0$ , the above equation gives  $\sigma_0 = 1 = \sigma_c$ , which is consistent with the static FBM results [1]. This analytic estimate overlaps with the data obtained from simulation (Fig. 6). It shows that the continuous and intermittent fracturing regimes are separated by a well defined phase boundary which depends on both, the stress level and the noise level [15].

In case of heterogeneous FBM where fibers have different strength thresholds, keeping in mind that in absence of noise  $T$ , we should always get  $\sigma_0 = \sigma_c$ , one can make a conjecture that

$$\sigma_0 \geq \frac{\sigma_c}{1 - T \log(1/N)}. \quad (51)$$

The numerical data for the heterogeneous cases (Fig. 6) having uniform and Weibull type fiber strength distributions supports the conjecture well [15].

Identification of such a phase boundary has important consequences in material-fracturing and in other similar fracture-breakdown phenomena. During material/rock fracturing, acoustic emission (AE) measurements can record the burst or avalanche events in terms of AE amplitude and AE energy [32]. Therefore, AE data could reveal the correct rupture-phase of a material body under stress. Once a system enters into continuous rupture phase the system-collapse must be imminent. Thus identification of rupture phase can guide us to visualize the final fate of a system. It can also help to stop system collapse, if it is possible to withdraw external stress in time -before the system enters into continuous rupture phase.

We will now discuss cooperative dynamics in both these regimes in the following sub-sections.

### A. Continuous breaking regime

In the continuous breaking regime one can describe the breaking dynamics in a FBM through a recursion relation [14]. Let us consider a homogeneous bundle having  $N$  fibers with exactly same strength thresholds 1; therefore critical (or failure) strength of the bundle is  $\sigma_c = 1$ . Now we consider a noise-induced failure probability for breaking of each fiber in the continuous regime:

$$P_f(\sigma, T) = \begin{cases} \frac{\sigma}{\sigma_c} \exp \left[ -\frac{1}{T} \left( \frac{x_i}{\sigma} - 1 \right) \right], & 0 \leq \sigma \leq x_i \\ 1, & \sigma > x_i \end{cases} \quad (52)$$

As all the fibers are identical,  $x_i = 1 = \sigma_c$ . The prefactor is a function of stress level  $\sigma$  and this is a careful choice to get a solution of the recursive dynamics, which we will describe below.

We denote the fraction of total fibers that remain intact at time (step)  $t$  by  $n_t$  and the breaking dynamics can be written as

$$n_{t+1} = n_t \left[ 1 - P_f \left( \frac{\sigma}{n_t}, T \right) \right]. \quad (53)$$

In the continuum limit the above recursion relation can be presented in a differential form

$$-\frac{dn}{dt} = \frac{\sigma}{\sigma_c} \exp \left[ -\frac{1}{T} \left( \frac{\sigma_c}{\sigma} n - 1 \right) \right]. \quad (54)$$

giving the failure time

$$t_f = T \exp \left( -\frac{1}{T} \right) \left[ \exp \left( \frac{\sigma_c}{\sigma T} \right) - 1 \right]. \quad (55)$$

The simulation result shows (Fig.7) exact agreement with this theoretical estimate.

In case of heterogeneous bundles where fibers have distributed strengths the failure times seem to follow another form [14]:

$$t_f = T \exp \left( -\frac{1}{T} \right) \left[ \exp \left( \frac{\sigma_c}{\sigma T} + \frac{1}{T} \right) - 1 \right]. \quad (56)$$

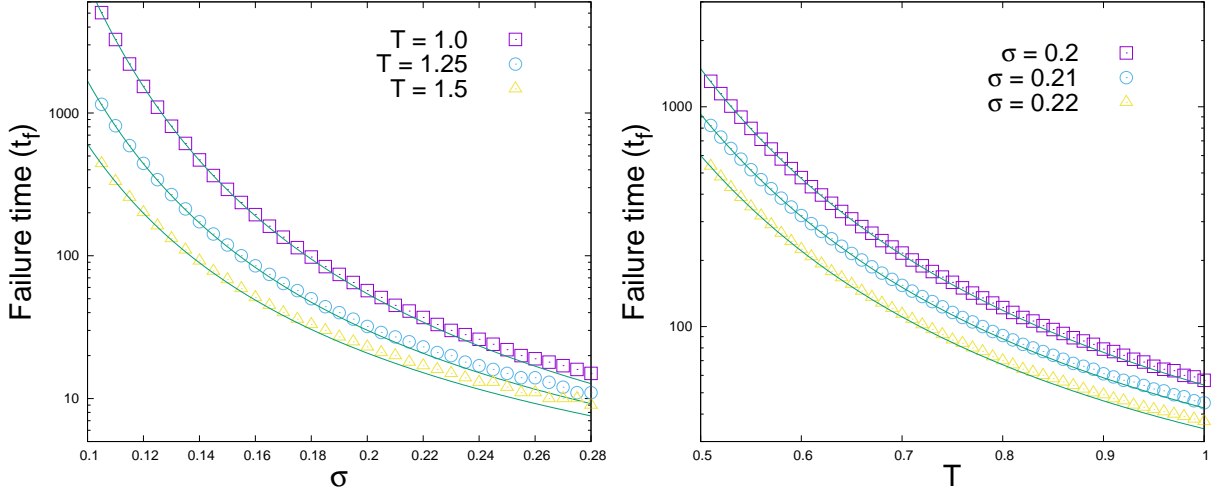


FIG. 7. Failure time vs.  $\sigma$  (left) and vs.  $T$  (right) for a homogeneous bundle having identical fibers with strength 1 ( $\sigma_c = 1$  as well). The data are for simulations over a single realization with system size  $N = 1000000$  and the solid lines are the theoretical estimates following Eq. (55).

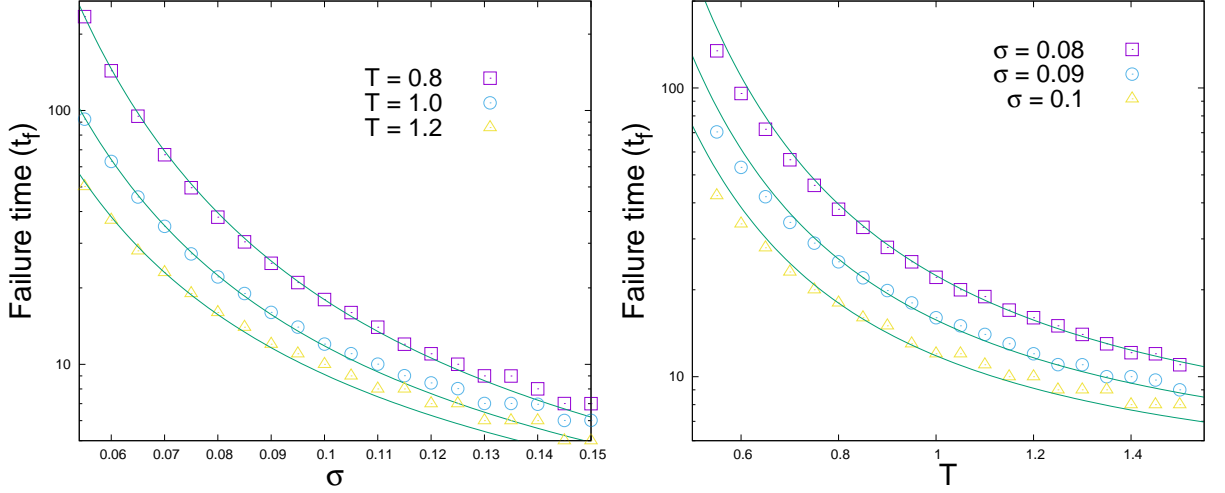


FIG. 8. Failure time vs.  $\sigma$  (left) and vs.  $T$  (right) for bundles having uniform strength distributions. The data are for simulations over 1000 realizations with system size  $N = 10^6$  and the solid lines are the theoretical estimates following Eq. (56).

This form was obtained through trial and error approach. It is extremely difficult (as of now) to write the recursion relation for noise-induced failure dynamics in case of heterogeneous systems. The simulation results have been compared with the formula above and the agreement (Fig.8) is quite satisfactory [14].

### B. Intermittent regime

As we discussed before, in the intermittent fracturing phase, simultaneous breaking events (avalanches) are separated by waiting times ( $t_W$ ) of different magnitude. The waiting time distribution can be fitted with a Gamma distribution [15] for both homogeneous and heterogeneous bundles

$$D(t_W) \propto \exp(-t_W/a)/t_W^{1-\gamma} \quad (57)$$

where  $\gamma = 0.15$  for homogeneous case and  $\gamma = 0.26$  for heterogeneous cases (Fig. 9). Here  $a$  is a measure of the extent of the power law regime and it seems that the power law exponent does not change with the variation of  $\sigma$ ,  $T$  and  $N$  [15].

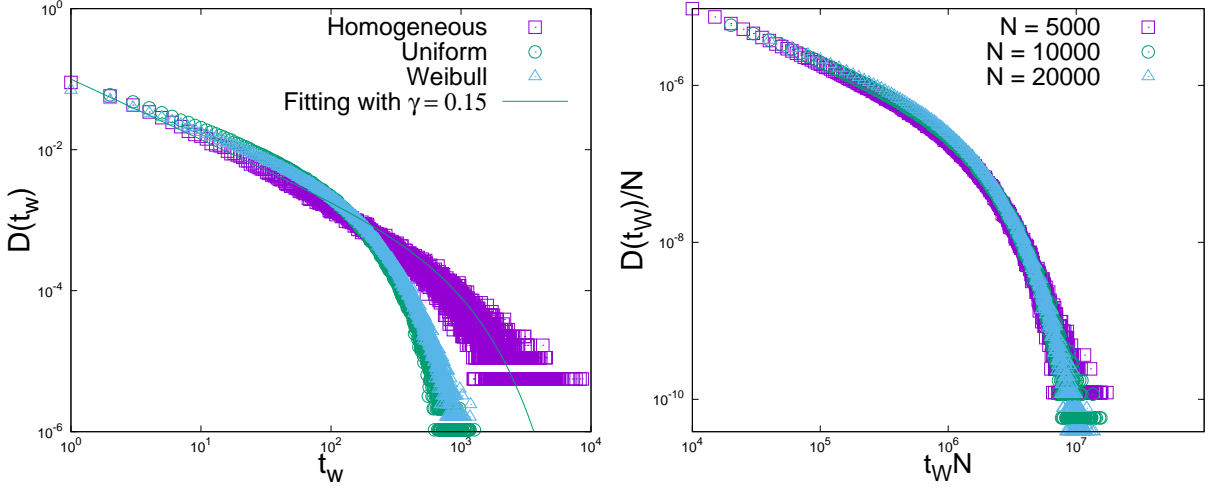


FIG. 9. Left: The simulation results for the waiting time distributions for three different type of fiber strength distributions with  $N = 20000$ . All the curves can be fitted with the Gamma form  $\exp(-t_W/a)/t_W^{1-\gamma}$ , where  $\gamma = 0.15$  for homogeneous case and  $\gamma = 0.26$  for uniform and Weibull distributions. Right: we show the data collapse of the waiting time distributions with system sizes for uniform fiber strength distribution.

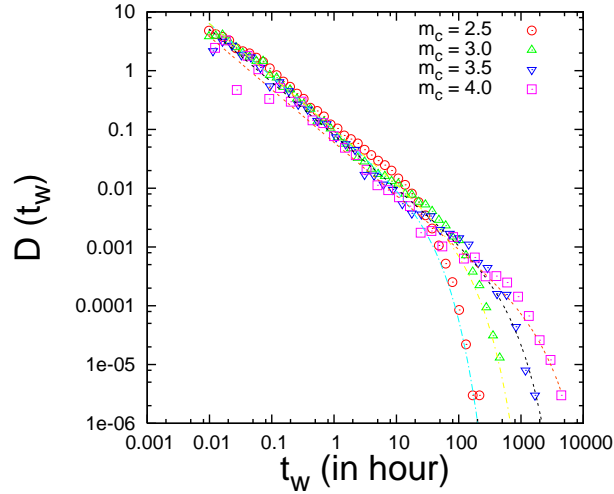


FIG. 10. Gamma-fitting (dotted lines) to the waiting time distributions in California catalog (1984-2002).

In the waiting time distributions, the power law part dominates for small  $t_W$  values and exponential law dominates for bigger  $t_W$  values. The inherent global load sharing nature is responsible for the power law part of the Gamma distribution, as power law usually comes from a long range cooperative mechanism [6, 33, 34]. The exponential part of the Gamma distribution is contributed by the noise induced failure factor  $P_f(\sigma, T)$ . For large  $t_W$  values one can eventually treat the failures to be independent. If  $P$  indicates the noise induced failure probability within  $t_W$  then the probability  $D(t_W) = A(1 - P)^{t_W N} \sim \exp(-Pt_W N)$ , where  $A$  is a constant. The normalization of  $D(t_W)$  requires  $A \sim N$ . Though for smaller values of  $t_W$ , one can not ignore the correlations between successive failures (responsible for the power law part in  $D(t_W)$ ), the exponential scaling behavior for  $D(t_W)$  can be easily obtained from the above. As shown in the inset of Fig. 9, the plot of  $D(t_W)/N$  against  $t_W N$  gives good data collapse for different  $N$  values. Such a data collapse indicates the robustness of the Gamma function form. It is not clear yet whether the Gamma type distribution is a direct consequence of the failure probability function (Eq. 48). It needs more investigations with various other types of possibilities for Eq. (48).

Apparently, the modeling scheme for noise-induced rupture process is not limited to any particular system, rather it is a general approach and perhaps it can model more complex situations like rupture driven earthquakes. In literature we can find evidences of stress-localization around fracture/fault lines in a active seismic-zone. Also, there

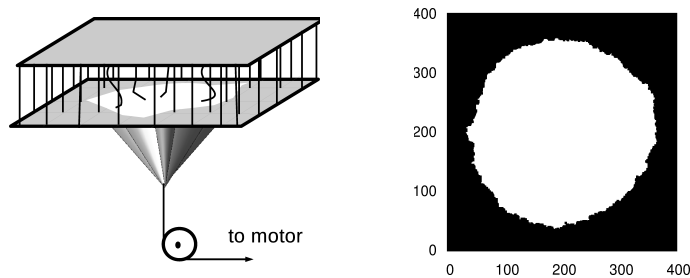


FIG. 11. A schematic representation of locally loaded fiber bundle model and the resulting interface propagation. From [39].

are several factors that can help rupture evolution, like friction, plasticity, fluid migration, spatial heterogeneities, chemical reactions etc. To some extent, such stress redistribution/localization can be taken into account through a proper load sharing scheme and a noise term ( $T$ ) can in principle represent the combined effect of all other factors.

To compare the waiting time results of the model system with real data, the California earthquake catalog from 1984 to 2002 [35] has been analyzed [15] to study the statistics of waiting times [36–38] between earthquake events. First, a cutoff ( $m_c$ ) has been set in the earthquake magnitude - so that all earthquake events above this cutoff magnitude will be considered for the analysis. The distribution of waiting times shows similar variation for different cutoff values. It seems [15] waiting time distributions for all the data sets follow a Gamma distribution [36]:

$$D(t_W) \propto \exp(-t_W/a)/t_W^{(1-\gamma)}; \quad (58)$$

with same  $\gamma$  ( $\simeq 0.1$ ) and different  $a$  values for different cutoff levels:  $a = 30, 120, 500, 2000$  respectively for  $m_c = 2.5, 3.0, 3.5, 4.0$  (see Fig. 10 ).

The similarities in waiting time statistics and scaling forms suggest that slowly driven (noise-induced) fracturing process and earthquake dynamics (stick-slip mechanism) perhaps have some common origin.

#### IV. INTERFACE PROPAGATION IN THE FIBER BUNDLES: SELF-ORGANIZATION AND DEPINNING TRANSITION

So far we have considered FBM versions that are globally loaded i.e., all the fibers in the system are loaded equally from the initial time, and the load remains equal on each surviving fiber, given that the load sharing is equal. This necessarily imply that the damage or failures in the system could occur at any point; indeed there is no notion of distance in this form of the model.

However, in fracture dynamics, particularly in the mode-1 variant of it, a front could propagate in the direction transverse to that of the loading. A fracture front necessarily implies damage localization within a region with a lower dimension than that of the system i.e., a front-line in two dimensions or a front surface in a three dimensional system. Indeed, driven front propagation through a disordered medium is not limited to fracture, but also happens in vortex lines in superconductors [61], magnetic domain walls in magnetic materials with impurities [62], contact line dynamics in wetting [63] and so on.

In the context of FBM, it is possible to capture the dynamics of a front propagating through a disordered medium by considering a localized loading of the system (when the fibers are arranged in a square lattice and the load is applied at an arbitrarily chosen central site; see Fig. 11) in dimension higher than one (in one dimension the damage interface is a point and hence cannot increase). The external load is increased at a low and constant rate (maintaining the separation of time scales between applied loading rate and redistribution process) [39]. Initially the system is not loaded anywhere except for the one fiber at an arbitrarily chosen central site. As the external load increased beyond the failure threshold of that central fiber, it breaks and the load carried by that fiber is redistributed among the fibers that are in the damage boundary (in the beginning just the four nearest neighbors). Therefore, the fibers that are newly exposed to the load after an avalanche, carry a lower load compared to those accumulating loads from the earlier avalanches. This process keeps a compact structure of the cluster of the broken fibers. The localized nature of the load redistribution is justified from the fact that the newly exposed fibers are further away from the point of loading and therefore carry a smaller fraction of the load at the original central site.

As the damage perimeter increases, so does the number of fibers on that perimeter. This implies that for an avalanche, the load per fiber will decrease along the damage boundary. But due to further increase in the load, this value will subsequently increase, initiating another avalanche. In the steady state, the load per fiber value will fluctuate around a constant and the system is said to have reached a self-organized state. In this state, the failure of

fibers in the process of avalanches have a scale free size distribution, which suggests that it is a self-organized critical (SOC) state (where external drive and dissipation balance and the critical point becomes an attractive fixed point [31]).

The steady state value of the load per fiber and the corresponding avalanche size distribution can be calculated for a variant of this model where the load redistribution is uniform along the entire damage boundary i.e. every fiber along the damage boundary gets the same fraction of load in a redistribution process. We discuss this for the Weibull distribution below, but this is true for other distributions as well.

The Weibull distribution in its general form can be written as

$$W_{\alpha,\beta}(x) = \alpha\beta x^{\alpha-1} e^{-\beta x^\alpha}, \quad (59)$$

where  $\alpha$  and  $\beta$  are the two parameters. We can consider the particular case when  $\alpha = 2$  and  $\beta = 1$ . The failure threshold of a fiber is greater than  $x$  with a probability that is proportional to  $\int_x^\infty x' e^{-x'^2} dx' \sim e^{-x^2}$ . Given that the probability density function for force is uniform, the probability of a fiber having load between  $x$  and  $x + dx$  is  $e^{-x^2} P(x) dx$ , with  $P(x) = c$  (unnormalized). The normalization gives  $c \int_0^\infty e^{-x^2} dx = 1$  implying  $c = \frac{2}{\sqrt{\pi}}$ . Hence the normalized probability density function for the load on the surviving fibers is

$$D_\sigma(x) = \frac{2}{\sqrt{\pi}} e^{-x^2}. \quad (60)$$

Similarly, the probability that the load is lower than  $x$  is proportional to  $x$ . Using the form for threshold distribution ( $\sim x e^{-x^2}$ ), the probability density function for threshold distribution of the survived fibers becomes

$$D_{th}(x) = \frac{4}{\sqrt{\pi}} x^2 e^{-x^2}. \quad (61)$$

Both of these functions are in good agreement with numerical simulations. Also the saturation value of the average load per fiber can be calculated as

$$\int_0^\infty x D_\sigma(x) dx = \frac{2}{\sqrt{\pi}} \int_0^\infty x e^{-x^2} dx = \frac{1}{\sqrt{\pi}}, \quad (62)$$

which is again in good agrees with simulations.

The size distribution of avalanches is a power law with the exponent value close to 3/2 (see Fig. 12), which is in agreement with the scaling prediction of avalanche size distributions in SOC models for mean field. The distribution of the avalanche duration i.e., the number of redistribution steps for an avalanche, is a power-law with exponent value close to  $2.00 \pm 0.01$ . which is again in agreement with scaling predictions of SOC models in mean field.

For estimating the avalanche size exponent, it can be assumed that the average load per fiber on the damage boundary has a distribution which is Gaussian around its mean:  $P(\sigma) \sim e^{-(\sigma-\sigma_c)^2/\delta\sigma}$ . Hence, from a dimensional analysis, mean-squared fluctuation  $\delta\sigma \sim (\sigma - \sigma_c)^2$ . Also the avalanche size  $S$  scales as  $(\delta\sigma)^{-1}$  since it may be viewed as the number of broken fibers after a load increase of  $\delta\sigma$ . This gives

$$(\sigma - \sigma_c) \sim S^{-1/2}. \quad (63)$$

The probability of an avalanche being of the size between  $S$  and  $S + dS$  is  $D(S)dS$ . Now, the deviation from the critical point scales [1] with the cumulative size of all avalanches upto that point; giving  $(\sigma - \sigma_c) \sim \int_S^\infty D(S)dS$ . If we take  $D(S) \sim S^{-\gamma}$ , then

$$(\sigma - \sigma_c) \sim S^{1-\gamma}. \quad (64)$$

Comparing Eqs. (63) and (64) therefore we have  $\gamma = \frac{3}{2}$ . So the probability density function for the avalanche size becomes  $D(S) \sim S^{-3/2}$ , which fits well with simulation results (Fig. 12).

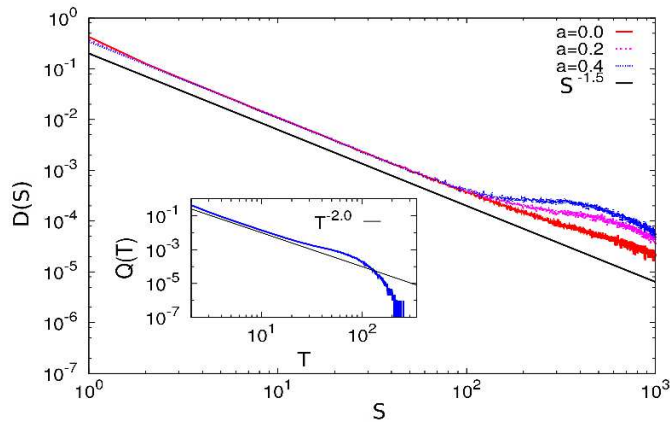


FIG. 12. The avalanche size distributions are plotted for zero and finite lower cut-offs for Model II. The distribution function is a power-law with exponent value  $1.50 \pm 0.01$ , which is also our estimate from scaling arguments. Inset: The distribution of avalanche duration is plotted for Model II. This also shows a power-law decay with exponent value  $2.00 \pm 0.01$ . From [39].

## V. SOME RELATED WORKS ON THE DYNAMICS OF FBM

In this section we would like to bring attention to some related works on the dynamics of FBM which, we believe, may be regarded as essential reading in this field.

As we have discussed in detail in the earlier sections, there has been considerable progress in characterizing the failure dynamics in the fiber bundle model through tools describing critical phenomena. One crucial step towards that direction is to identify the universality class of the model. That often needs a coarse grained description of the model, writing down the free energy form suited for the dynamics and then identifying the symmetries and consequently the universality class. One such step was done in Ref. [43] by writing down a mesoscopic description of the ELS-FBM. Specifically, writing the time evolution of the order parameter  $n(\sigma) - n_c = \eta$  and the driving field (stress increase) as  $J = \sigma_c - \sigma$ , the dynamics is described by

$$\frac{\partial \eta}{\partial t} = -\eta^2 + J. \quad (65)$$

Writing in terms of the density of intact fibers  $n$ ,

$$\frac{\partial n}{\partial t} = \lambda n(1 - n) - \sigma, \quad (66)$$

with  $\lambda = 1$ . This equation has a particle-hole symmetry for zero external field  $\sigma = 0$ , hence generally expected to be in the CDP or compact domain growth universality class of non-equilibrium phase transition [44]. Although done for the ELS version, this approach of relating fiber bundle model dynamics to nonequilibrium critical phenomena through a Langevin equation could provide useful insights in more realistic versions.

Among other attempts to relate fracture and in particular FBM dynamics with different universality classes, a relatively less explored route is that of the hydrodynamics of turbulence. The analogy between the velocity fluctuation in turbulence and surface roughness due to fracture have been explored before (see e.g., [51]). However, given that FBM is able to provide a reasonably consistent picture for fracture dynamics, its association with hydrodynamics of fracture is a crucial question. In Ref. [52] the relation between the Kolmogorov energy dispersion in turbulence and avalanche dynamics in the FBM was explored. Specifically, the vortex lines in a fully developed turbulence can be mapped to Self Avoiding Walk (SAW) picture of polymers [53]. Then following Flory's theory [54], the Kolmogorov energy dispersion becomes

$$E_q \sim q^{-1/\nu_F}, \quad (67)$$

where  $q$  is the wave number,  $\nu_F$  is the Flory exponent and  $d$  is the spatial dimension. Then drawing the parallel with the energy dispersion in avalanche dynamics in the FBM (see Eq. (47)), we get  $E_q \sim q^{-d/3}$  for the mean field case (i.e.  $d = d_u$ , the upper critical dimension). By taking  $d_u = 6$ , which is consistent for the FBM [26], we get back the Flory mean field result  $E_q \sim q^{-2}$ . In parallel, by taking the correlation length as inverse of the wave number  $q$ , and

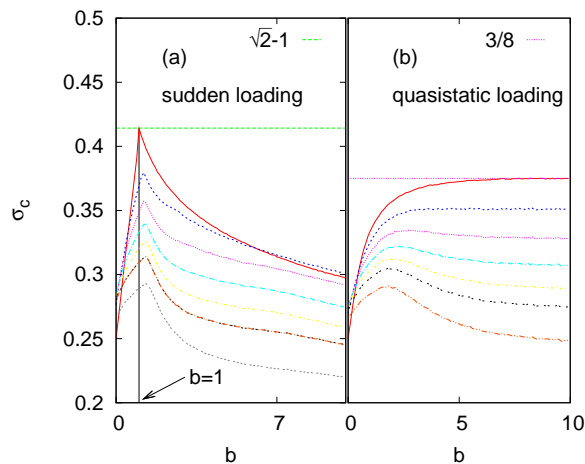


FIG. 13. The phase diagram in the  $b - \sigma_c$  plane ( $b$  represents the anisotropy in the load redistribution process) is shown for (a) discrete step and (b) quasi-static loading for various fractional errors in the knowledge of the threshold values of the individual fibers (curves from top to below are for  $e = 0.0, 0.1, 0.2, 0.3, 0.4, 0.5, 0.75$ ). The upper bounds for both cases are shown which are reached for  $b = 1$  (a) and  $b \rightarrow \infty$  (b). From [45]

using finite size scaling arguments, one can show that  $\nu d = 2/3$  in the mean field limit, where  $\nu$  is the correlation length exponent. Again using  $d = 6$  as the upper critical dimension, one gets  $\nu = 1/4$ .

It may be noted that there is also a gratifying consistency in the main results discussed above. In the ELS FBM, the critical exponents  $\beta$ ,  $\gamma$  and  $\nu$  for the order parameter, breakdown susceptibility and correlation length respectively satisfy the Rushbrooke scaling relation (incorporating the hyperscaling relation) [64]:  $2\beta + \gamma = d\nu$ , with  $\beta = 1/2 = \gamma$  and with the value of the upper critical dimension  $d = 6$  and  $\nu = 1/4$ .

Given that the fiber bundle is essentially an ensemble of discrete elements having finite failure thresholds, under the condition of conserved load, it can serve as a generic model for intermittent progress towards catastrophic failure in a wide variety of systems. Such systems can be roads carrying traffic, power grids to redundant computer circuitry. In several of such cases, the load redistribution following the failure of an individual element (say, traffic jam along one road, failure of one power station etc.), is controllable to some extent - a freedom lacking in the case of stressed disordered solids. Under such circumstances, it is useful to ask the question how the total load carrying capacity of the system could be maximized by a suitable load redistribution rule [45].

It is rather straightforward to establish that the maximum limit of  $\sigma_c$  would be achieved, when the maximum number of fibers carry load to their fullest capacity. For a uniform distribution of the failure thresholds in  $(0,1)$ , it is possible to show that for loading in a discrete step the limiting value for the critical load is  $\sqrt{2} - 1$  and for quasi-static loading it is  $3/8$ . The remaining question, therefore, is to find the rule of load transfer following a local failure that can achieve the global failure threshold in the closest proximity to the above mentioned limits. Intuitively, it is clear that a higher share of load should be transferred to the fibers with higher capacity. Generally, it is useful to assume that the transfer rule would be of the form  $A(f_i - \sigma_i)^b$ , where  $f_i$  and  $\sigma_i$  are respectively the failure threshold and load of the  $i$ -th element,  $A$  is an appropriate constant to ensure load conservation and  $b$  is a parameter.

The dynamics, as discussed before, depends on whether the load is applied in a discrete step or gradually. The maximization of the strength of the system would also, therefore, depend on the loading protocol. The only parameter to tune here is  $b$ . It is possible to calculate analytically that the maximum strength is indeed achieved with this redistribution rule for  $b = 1$  for the discrete step loading and  $b \rightarrow \infty$  (practically achieved for  $b \approx 10$ ) for quasi-static loading (see Fig. 13).

An important information in implementing the redistribution rule is the exact knowledge of the failure thresholds of all the surviving elements. This requirement may not be always fulfilled. Assuming that there is a (fractional) error  $e$  in the knowledge of the failure thresholds, numerical simulations show (see fig. 13) that the redistribution rule still gives better results than a uniform redistribution. Therefore, in the situations where the load redistribution is controllable, the redistribution rule mentioned above give the best possible outcome.

We like to mention that cooperative dynamics appears in another class of Fiber Bundle Models where fibers are treated as viscoelastic elements [57–59]. The readers can go through [60] (appearing in the same Research Topic: The Fiber Bundle) for a review on viscoelastic Fiber Bundle Models.

## VI. SUMMARY AND CONCLUSIONS

One can easily see, the fiber bundle model (FBM), introduced by Peirce [5] in 1926 as a model to understand the strength of composite materials, is an extremely elegant one. As mentioned before, the model consists of a macroscopically large number of parallel fibers/springs with linear elastic behavior and of identical length. The breaking thresholds, however, are different for each fiber and are drawn from a probability distribution. All these fibers/springs hang from a rigid horizontal platform. The load on the bundle is applied at the lower horizontal platform. This lower platform has been assumed here to be rigid, implying the stress or load-share per surviving fibers/springs is equal, irrespective of how many fibers or springs might have broken (equal load sharing or ELS scheme). It may be mentioned that we have not discussed here the extensive studies on fiber bundle models with Local Load Sharing (LLS) schemes, for which the readers may be advised to consult Refs. [1] and [28] and the ‘impregnated fiber bundle’ models, for which the readers may be referred to the Refs. [65, 66].

As discussed in this review, the failure dynamics of the of FBM under ELS scheme of load sharing have been analyzed for long, both analytically as well as numerically by several distinguished groups of investigators from engineering, physics and applied mathematicians. The results may be briefly summarized as follows: After introducing the model, we have described the dynamics of the equal load sharing (ELS) fiber bundle model in sec. II. Specifically, In this section we discuss and summarize works (Refs. [1, 2, 4, 8, 28]) related to the cooperative failure dynamics in the ELS fiber bundle model having large number of fibers with different strength thresholds. We start this section by describing the force displacement relation (load curve) when the bundle is stretched by an amount  $x$ . The maximum point of this curve gives the strength of the whole bundle. One can easily derive the strength of the bundle for different fiber threshold distributions. We have chosen uniform and Weibull distributions as examples and derive bundle’s strength as critical displacement ( $x_c$ ) and critical force ( $F_c$ ). Next we describe how to formulate the dynamics of failure through a recursion relation in case of loading by discrete steps when fiber thresholds are uniformly distributed. The solution of the recursion relation at the fixed point gives some important information of the failure dynamics: Order parameter goes to zero following a power law as the applied stress values approaches critical value and both susceptibility and relaxation time diverge at the critical stress following well defined power laws. To check the universality of the failure dynamics we choose different type of fiber strength distribution (linearly increasing) and derive the fixed-point solutions. The exponent values of the power laws for order parameter, susceptibility and relaxation time variations are exactly the same as the model with a uniform distribution and therefore the failure dynamics in ELS fiber bundle model is universal. In addition, we present the exact solutions for pre and post-critical relaxation behavior which we believe is one of the most important theoretical developments in this field. At the last part of this section we present an analysis on the avalanche statistics for loading by fixed amount. Such a loading scheme introduces a different mechanism for the avalanche sizes of simultaneous breaking of fibers. We discuss using analytical calculations that the exponent of the avalanche size distribution ( $P(S)$ ) for discrete loading would be  $-3$ , which is different ( $-5/2$ ) from the same in case of quasi-static loading situation [6].

In section III, we summarize some recent developments (Refs. [11–16]) on the cooperative dynamics of noise-induced failure in ELS fiber bundle models. In addition to applied stress, the noise factor plays a crucial role in triggering failure of individual fibers. The trick here is how to define the failure probability of individual fibers as a function of applied/effective stress and the noise level. Normally noise-level remains constant during the entire failure process, but the stress level increases gradually due to stress redistribution mechanism. The choice of the probability function should satisfy the fact that without noise factor the noise-induced failure model must reproduce the classical failure scenario (discussed in section II). We start this section by presenting a noise-induced failure probability for individual fiber failure. The choice of stress and noise level dictates whether the system is in continuous breaking regime or in intermittent breaking regime. Through a mean-field argument, one can easily find out the phase diagram separating these two regimes (Eq. (50), Fig. 6). Apparently, the continuous breaking regime is easy to analyze. For homogeneous bundle, where all the fibers are identical (strengths are same), one can write down the failure dynamics as a recursion relation (Eq. (53)). The solution gives an exact estimate for the failure time (steps) as a function of applied stress ( $\sigma$ ) and noise level ( $T$ ) (Eq. (55)). Simulation results show perfect agreement with the theoretical estimates (Fig. 7). When we consider a strength distribution among the fibers in the model, it becomes extremely difficult to construct the recursion relation for the failure dynamics. One reason could be that during the failure process the strength distribution gets changed with time. However, the simulation results (Fig. 8) for the failure time of heterogeneous bundles follow similar variation with applied stress and noise level with an extra noise factor (Eq. (56)). Next we discuss the other regime, i.e., the intermittent failure regime where there are waiting time between two failure phases. The distribution of waiting time is the most important aspect in this regime. Simulation results on homogeneous and heterogeneous bundles show that the waiting time distribution follows a Gamma distribution (Eq. (57)) and a data-collapse confirms the universal nature of such distribution function (Fig. 9). Surprisingly, waiting time distribution from earthquake time series (California catalog) seem to follow similar Gamma distribution (Fig. 10).

In section IV, we have considered self-organized fracture front propagation in a fiber bundle model where the

fracture front adjusts its size in a self-organized way to meet the increasing load on the bundle and several features of the self-organized dynamics can still be analyzed in a mean field way; see, e.g., Fig. 12 for the avalanche size distribution which fits well with  $D(S) \sim S^{-3/2}$ .

As mentioned already (in section II), the universality class of the dynamics of fixed load increment during the ongoing dynamics of failure in the bundle (until its complete failure) will be different from that for the quasi-static (or weakest link failure type) loading during its dynamics. And, as discussed in section V, it is given by the Flory statistics for linear polymers, when fracture dynamics in the bundle is mapped to turbulence and one utilizes the Kolmogorov type dispersion energy cascades [52]. In particular, we obtained already ([3]; see Eqns. (35) and (36)) the order parameter exponent  $\beta = 1/2 = \gamma$ , the susceptibility exponent. Employing the Rushbrooke scaling  $2\beta + \gamma = d\nu$  (where  $\nu$  denotes the correlation length exponent), we get  $d\nu = 3/2$  here in conformity with finite size scaling results. As discussed in [52] (see also the discussions in section V), mapping the avalanche size distribution (Eq. (47)) to the Kolmogorov energy dispersion in turbulence (Eq. (67)), identifying  $S$  with the energy and inverse correlation length as the wave vector  $q$ , we got the upper critical dimension  $d_u$  for FBM in the ELS scheme to be 6. This suggests the correlation length exponent  $\nu$  value here to be  $1/4$ .

As discussed in this review, the absence of stress concentrations or fluctuations around the broken fibers allows mean-field type statistical analysis in such Equal Load Sharing Fiber Bundle Models. This feature of the models helped major analytical studies for the breaking dynamics and also allowed precise comparisons with computer simulation results.

## VII. ACKNOWLEDGMENTS

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